## INCITE summer school 2017

IRP32: A new modelling approach for stabilisation of smart grids

Felix Koeth<br>G2Elab Grenoble

June 30, 2017

This project has received funding from the European Union's Horizon 2020 research and innovation programme under Marie Sklodowska-Curie grant agreement No 675318

## Outline

1. Motivation and introduction

## 2. Properties of the DAE model

3. Matrix structures

## 4. Appenix: Singularity of jacobian submatrices

## Power studies and synchronization

- Stable operation of the power system depends on the ability of the power system to synchronize
- Synchronization is also found in other physical systems, like biological, mechanical or chemical oscillators
- In simplified power system models, sophisticated synchronization conditions can be found.
- Main goal of my work: Expand the models and try to expand current synchronization conditions for this more complex models


## Synchronization - I

- Synchronization in dynamical systems refers to a coordinate behavior
- All oscillators rotate with a common frequency
- Angular differences are bounded
- Corresponds to the equilibrium solution to dynamical models
- Stability of synchronized solutions if equilibrium is stable


## Synchronization - II

If anyone is interested in synchronization:


Or wait for my blog entry this month ...

## Structure-preserving model and previous results

One of the most commonly simplified model to study the power system dynamics is the structure-preserving model:

$$
\begin{align*}
M_{i} \ddot{\theta}+D_{i} \dot{\theta}=\omega_{i, \mathrm{p}}+\underbrace{\sum_{j} V_{i} V_{j} B_{i j} \sin \left(\theta_{i}-\theta_{j}\right)}_{P_{e, g}} \quad i \in \mathcal{V}_{\mathcal{G}}  \tag{1}\\
D_{i} \dot{\theta}=\omega_{i, \mathrm{p}}+\sum_{j}^{\sum_{i} V_{j} B_{i j} \sin \left(\theta_{i}-\theta_{j}\right)} \quad i \in \mathcal{V}_{\mathcal{L}} \tag{2}
\end{align*}
$$

For this model, the existence and stability of a synchronized solution is given if $[1]^{1}$ :

$$
\begin{equation*}
\left\|L^{\dagger} \omega\right\|_{\varepsilon, \infty} \leq 1 \tag{3}
\end{equation*}
$$

[^0]
## Reactive power

- The structure-preserving model neglects reactive power and voltage dynamics
- Especially for load buses, reactive power flow will have a serious impact on the voltage magnitude
- The voltage magnitude at each bus influences the coupling strength of the network, and thus the synchronization properties
- Modeling the reactive power and treating the (load bus) voltage magnitudes as variables results in a DAE system with the algebraic constraint:

$$
\begin{equation*}
Q_{i}=-\sum_{j} V_{i} V_{j} B_{i j} \cos \left(\theta_{i}-\theta_{j}\right) \tag{4}
\end{equation*}
$$

## Full model

- Proposed model: Model generators with the swing equation (as PV buses) and loads as constant power loads
- At load bus, voltage magnitude and phase are algebraic variables (as PQ buses)

$$
\begin{gather*}
M_{i} \ddot{\theta}+D_{i} \dot{\theta}=\omega_{i, \mathrm{p}}+\sum_{j} V_{i} V_{j} B_{i j} \sin \left(\theta_{i}-\theta_{j}\right) \quad i \in \mathcal{V}_{\mathcal{G}}  \tag{5}\\
P_{i}=\sum_{j} V_{i} V_{j} B_{i j} \sin \left(\theta_{i}-\theta_{j}\right) \quad i \in \mathcal{V}_{\mathcal{L}}  \tag{6}\\
Q_{i}=-\sum_{j} V_{i} V_{j} B_{i j} \cos \left(\theta_{i}-\theta_{j}\right) \tag{7}
\end{gather*}
$$

## Problems with DAE

- Plans for the extended model
- Numerical simulations
- Finding equilibrium points
- Calculate stability of equilibrium points
- For a solution, we need consistent initial conditions $\rightarrow$ equilibrium points
- Existence of solutions is not always guaranteed, even for consistent initial conditions


## Loadability condition

- In steady state, the full model corresponds to the full load-flow equations, which have to fulfill the loadability limit [2]
- The limit of the loadability is given by $y^{*}$, which can be found by finding:

$$
\operatorname{det} J_{y^{*}}=\operatorname{det}\left(\begin{array}{ll}
\frac{\partial P}{\partial \theta} & \frac{\partial P}{\partial V} \\
\frac{\partial Q}{\partial \theta} & \frac{\partial Q}{\partial V}
\end{array}\right)_{y^{*}}=0
$$



## Small signal stability

- Studying the behavior around an equilibrium point (where the loadability limit is valid) by linearization
- With the error variables $\tau_{i}=\theta_{i}-\theta_{i}^{*}$ and $\nu_{i}=V_{i}-V_{i}^{*}$.

$$
\begin{equation*}
\binom{M_{i} \ddot{\tau}_{i}+D_{i} \dot{\tau}_{i}}{0}=J_{y^{*}}\binom{\tau}{\nu} \tag{8}
\end{equation*}
$$

Again, the jacobian matrix plays an important role in the dynamics of the full model.

## Jacobian of load-flow equations

$$
\begin{aligned}
& \frac{\partial P_{i}}{\partial \theta_{j}}= \begin{cases}\sum_{j} V_{i}^{*} V_{j}^{*} B_{i j} \cos \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i=j \\
-V_{i}^{*} V_{j}^{*} B_{i j} \cos \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i \neq j\end{cases} \\
& \frac{\partial P_{i}}{\partial V_{j}}= \begin{cases}\sum_{j} V_{j}^{*} B_{i j} \sin \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i=j \\
V_{i}^{*} B_{i j} \sin \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i \neq j\end{cases} \\
& \frac{\partial Q_{i}}{\partial \theta_{j}}= \begin{cases}-\sum_{j} V_{i}^{*} V_{j}^{*} B_{i j} \sin \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i=j \\
V_{i}^{*} V_{j}^{*} B_{i j} \sin \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i \neq j\end{cases} \\
& \frac{\partial Q_{i}}{\partial V_{j}}= \begin{cases}\sum_{j} V_{i}^{*} V_{j}^{*} B_{i j} \cos \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i=j \\
V_{i}^{*} V_{j}^{*} B_{i j} \cos \left(\theta_{i}^{*}-\theta_{j}^{*}\right), & \text { if } i \neq j\end{cases}
\end{aligned}
$$

With Laplacian and non-laplacian structure.

## Laplacian structure

- Laplacian of graph is a common tool used in graph theory. Encodes the structure of the grid
- For a weighted graph with weights $a_{i j}$ between vertex $i$ and $j$, the laplacian matrix is given as:

$$
L=\left(\begin{array}{ccccc}
\sum_{j} a_{0 j} & -a_{01} & -a_{02} & \cdots & -a_{0 n}  \tag{9}\\
-a_{10} & \sum_{j} a_{1 j} & -a_{12} & \cdots & -a_{1 n} \\
\vdots & \vdots & \vdots & \vdots & \vdots \\
-a_{n 0} & -a_{n 1} & -a_{n 2} & \cdots & \sum_{j} a_{n j}
\end{array}\right)
$$

- $L$ is a symmetric matrix (only real eigenvalues) with the non-degenerate eigenvalue $0^{2}$
- The laplacian is linked to the consensus protocol and the dynamics of the linearized load-flow equations for the active power.

[^1]
## Other submatrix type

- The other Jacobian submatrix has a related structure to the Laplacian matrix, with positive off-diagonal elements:

$$
M=\left(\begin{array}{ccccc}
\sum_{j} a_{0 j} & a_{01} & a_{02} & \cdots & a_{0 n}  \tag{10}\\
a_{10} & \sum_{j} a_{1 j} & a_{12} & \cdots & a_{1 n} \\
\vdots & \vdots & \vdots & \vdots & \vdots \\
a_{n 0} & a_{n 1} & a_{n 2} & \cdots & \sum_{j} a_{n j}
\end{array}\right)
$$

- For a symmetric matrix $A, M$ is also symmetric. It is weakly diagonally dominant. In contrast to the laplacian, it is not always singular, depending on the structure of the graph.


## Singularity properties

Singularity of matrices: Matrix is non-invertible, the determinant is zero, the matrix has a zero eigenvalue Nonsingular matrices are invertible!

- Full graph: nonsingular
- Ring graph: singular if $n$ even, nonsingular if $n$ odd
- Random graphs:
- Erdős-Rényi graph graph: Nonsingular for $N>20$
- Random geometric graph: Nonsingular
- Watts-Strogats graph: Singular in $\approx 50 \%$ of cases.


## Outlook

- Analytical treatment: Possible, impossible? Are there good ways to compare the Laplacian matrices with the almost-laplacian matrices M?
- The small signal model may be solved in the spectral domain, as was done for the constant voltage case in [3]. For that, the matrix properties of the jacobian, and especially the submatrices have to be studied.
- Concentrating on numerical simulations? Instabilities observed in the simulation, need to simulate control?


## Thanks for your attention! <br> Any questions?

## Bibliography I

[1] F. Dorfler, M. Chertkov, and F. Bullo. "Synchronization in complex oscillator networks and smart grids". In: Proceedings of the National Academy of Sciences 110.6 (Feb. 5, 2013), pp. 2005-2010.
[2] T. van Cutsem and K. Vournas Costas. Voltage Stability of Electric Power Systems. Kluwer international series in engineering and computer science. Springer, 1998.
[3] Nicolás Rubido. Energy Transmission and Synchronization in Complex Networks. Springer Theses. Cham: Springer International Publishing, 2016.
[4] Savoie J. Dubeau F. "A remark on cyclic tridiagonal matrices". eng. In: Applicationes Mathematicae 21.2 (1991), pp. 253-256.

## Singularity of $M-1$

Percentage of singular matrices $M$, for different weighted random graphs models (Watts-Strogatz graph WSG, Erdős-Rényi graph ERG and random geometric graphs RGG) and different realizations. Here, $N$ is the number of nodes and $p$ is the rewiring probability/radius. The Watts-Strogats graph is initially connected to two nearest neighbors.

| $N$ | $p$ | WSG | ERG | RGG |
| :---: | :---: | :---: | :---: | :---: |
| 10 | 0.15 | 54.16 | 32.1 | - |
| 10 | 0.3 | 45.445 | 3.86 | 1.58 |
| 10 | 0.6 | 38.3 | 0.0 | 0.0 |
| 10 | 0.75 | 38.08 | 0.0 | 0.0 |
| 20 | 0.15 | 48.58 | 0.44 | - |
| 20 | 0.3 | 46.54 | 0.0 | 0.0 |
| 20 | 0.6 | 44.96 | 0.0 | 0.0 |
| 20 | 0.75 | 44.16 | 0.0 | 0.0 |

## Singularity of $M$ - II

| $N$ | $p$ | WSG | ERG | RGG |
| :---: | :---: | :---: | :---: | :---: |
| 30 | 0.15 | 47.94 | 0.0 | - |
| 30 | 0.3 | 48.19 | 0.0 | 0.0 |
| 30 | 0.6 | 45.28 | 0.0 | 0.0 |
| 30 | 0.75 | 44.58 | 0.0 | 0.0 |
| 60 | 0.15 | 49.88 | 0.0 | - |
| 60 | 0.3 | 48.28 | 0.0 | 0.0 |
| 60 | 0.6 | 46.7 | 0.0 | 0.0 |
| 60 | 0.75 | 47.62 | 0.0 | 0.0 |
| 120 | 0.15 | 50.96 | 0.0 | - |
| 120 | 0.3 | 49.6 | 0.0 | 0.0 |
| 120 | 0.6 | 47.36 | 0.0 | 0.0 |
| 120 | 0.75 | 47.72 | 0.0 | 0.0 |

## Singularity of $M$ - III

For complete graphs with $N$ edges, $M_{F, N}$ is given by:

$$
M_{F, N}=\left(\begin{array}{ccccc}
N-1 & 1 & 1 & \cdots & 1 \\
1 & N-1 & 1 & \cdots & 1 \\
\vdots & \vdots & \vdots & \vdots & \vdots \\
1 & 1 & 1 & \cdots & N-1
\end{array}\right)
$$

Testing for linear dependency with $x_{i}, i \in[0, N]$. Subtracting column $i$ from $j$ in the resulting linear system results in:

$$
\begin{array}{r}
(N-2) x_{i}-(N-2) x_{j}=0 \\
\forall i, j: x_{i}=x_{j} \rightarrow x_{i}=0
\end{array}
$$

So, all columns of $M$ are linear independent and $M_{F, N}$ is non-singular.

## Singularity of $M$ - IV

Ring graph with matrix $M_{R, n}$ : singular if $n$ even, not singular if $n$ odd!

$$
M_{R, n}=\left(\begin{array}{ccccc}
2 & 1 & 0 & \cdots & 1 \\
1 & 2 & 1 & \cdots & 0 \\
\vdots & \vdots & \vdots & \ddots & \vdots \\
1 & 0 & 0 & \cdots & 2
\end{array}\right) \quad \text { define: } K_{n}=\left(\begin{array}{ccccc}
2 & 1 & 0 & \cdots & 0 \\
1 & 2 & 1 & \cdots & 0 \\
\vdots & \vdots & \vdots & \ddots & \vdots \\
0 & 0 & 0 & \cdots & 2
\end{array}\right)
$$

For the tridiagonal matrix $K_{n}$ we have that $\operatorname{det} K_{n}=n+1^{3}$. According to [4], we can calculate the determinant of the cyclic tridiagonal matrix as:

$$
\begin{aligned}
\operatorname{det} M_{R, n}= & \operatorname{det} K_{n}+(-1)^{n+1}\left(\prod_{i=1}^{n} a_{i}+\prod_{i=1}^{n} c_{i}\right) \\
& -a_{1} c_{n} \delta_{n-1} \sum_{k=1}^{n-1} \frac{1}{\delta_{k-1} \delta_{k}}\left(\prod_{i=1}^{n} a_{i}\right)\left(\prod_{i=1}^{n} c_{i}\right)
\end{aligned}
$$

[^2]
## Singularity of $M-\mathrm{V}$

Here, $a_{i}=c_{i}=1$ and $\delta_{k}$ is the $k$-th leading principal minor of the matrix $K_{n}$. Removing the last $m$ rows and columns from $K_{n}$ results in the matrix $K_{n-m}$, thus $\delta_{k}=k+1$. With ${ }^{4}$,

$$
\sum_{k=1}^{n} \frac{1}{k(k+1)}=\frac{n}{n+1}
$$

we get:

$$
\operatorname{det} M_{R, n}=n+1+2 \cdot(-1)^{n+1}-(n-1)= \begin{cases}0, & \text { if } n \text { is even } \\ 4, & \text { if } n \text { is odd }\end{cases}
$$

Does this explain the results for the WSG? Is that actually useful? Other matrix properties?

[^3]
[^0]:    ${ }^{1}$ With the (pseudo-inverse) network laplacian $L$

[^1]:    ${ }^{2}$ For neglected reactive power and constant voltage magnitudes, the system is always at the loadability limit.

[^2]:    ${ }^{3}$ Because $\operatorname{det} K_{n}=\operatorname{det} K_{n-1}-\operatorname{det} K_{n-2}$

[^3]:    ${ }^{4}$ Might be well known, can be shown by simple mathematical induction.

